



Na bazi premera dela sastojine crnog bora u Lipovici, površine $p = 0.1$ ha i poznate starosti od 55 godina, odrediti i analizirati sledeće elemente rasta i sastojinske izgrađenosti i po potrebi ih grafički predstaviti:

1. Srednje prečnike i visine; 2. Temeljnice i zapremine;

2.1. Temeljnice pojedinačnih stabla, dobijene izrazom $g = \frac{d^2 \cdot \pi}{40000}$, upisivati u tabelu koja je u sklopu ovog zadatka.

2.2. Na osnovu stepene funkcije, $h = 7.4562591 \cdot d^{0.3017336}$, pomoću koja smo izravnali vezu prečnika i visine nacrtati visinsku krivu na grafikonu iz prethodnog zadatka. Takođe, na osnovu dobijene visinske krive, odrediti i upisati visine na mestima gde nedostaju u tabeli premera iz prethodnog zadatka.

–	d [cm]	+	v [m ³]
9.5	10	10.49	$0.003321 + 0.0019551 \cdot h + 0.000212 \cdot h^2 - 0.000008449883 \cdot h^3$
10.5	11	11.49	$0.019433 - 0.00197 \cdot h + 0.000608 \cdot h^2 - 0.000018 \cdot h^3$
11.5	12	12.49	$-0.032979 + 0.013841 \cdot h - 0.000671 \cdot h^2 + 0.000015 \cdot h^3$
12.5	13	13.49	$-0.018609 + 0.012202 \cdot h - 0.000566 \cdot h^2 + 0.000015 \cdot h^3$
13.5	14	14.49	$-0.044235 + 0.019489 \cdot h - 0.001044 \cdot h^2 + 0.000026 \cdot h^3$
14.5	15	15.49	$-0.019722 + 0.014333 \cdot h - 0.000514 \cdot h^2 + 0.000012 \cdot h^3$
15.5	16	16.49	$-0.007571 + 0.012104 \cdot h - 0.000137 \cdot h^2$
16.5	17	17.49	$0.01 + 0.01 \cdot h$
17.5	18	18.49	$0.223156 - 0.059532 \cdot h + 0.008337 \cdot h^2 - 0.000414 \cdot h^3 + 0.000007327232 \cdot h^4$
18.5	19	19.49	$0.013912 + 0.012462 \cdot h$
19.5	20	20.49	$0.017538 + 0.01378 \cdot h$
20.5	21	21.49	$-0.044633 + 0.031277 \cdot h - 0.001271 \cdot h^2 + 0.000032 \cdot h^3$
21.5	22	22.49	$0.023077 + 0.016703 \cdot h$
22.5	23	23.49	$0.026154 + 0.018297 \cdot h$
23.5	24	24.49	$0.03 + 0.02 \cdot h$
24.5	25	25.49	$0.0338462 + 0.0213187 \cdot h$
25.5	26	26.49	$0.042582 + 0.022802 \cdot h$
26.5	27	27.49	$-0.110769 + 0.057962 \cdot h - 0.002315 \cdot h^2 + 0.000052 \cdot h^3$
27.5	28	28.49	$-0.010869 + 0.038017 \cdot h - 0.000767 \cdot h^2 + 0.000017 \cdot h^3$
28.5	29	29.49	$0.232198 - 0.012326 \cdot h + 0.002885 \cdot h^2 - 0.000064 \cdot h^3$
29.5	30	30.49	$0.156749 + 0.00896 \cdot h + 0.001426 \cdot h^2 - 0.000029 \cdot h^3$
30.5	31	31.49	$0.088979 + 0.024003 \cdot h + 0.000711 \cdot h^2 - 0.000018 \cdot h^3$
31.5	32	32.49	$0.025502 + 0.036402 \cdot h + 0.000158 \cdot h^2 - 0.000007331993 \cdot h^3$
32.5	33	33.49	$-0.046558 + 0.051162 \cdot h - 0.000499 \cdot h^2 + 0.000003351768 \cdot h^3$
33.5	34	34.49	$-0.149239 + 0.07371 \cdot h - 0.001758 \cdot h^2 + 0.000029 \cdot h^3$
34.5	35	35.49	$-0.148236 + 0.077322 \cdot h - 0.001863 \cdot h^2 + 0.000031 \cdot h^3$
35.5	36	36.49	$-0.084291 + 0.07077 \cdot h - 0.001462 \cdot h^2 + 0.000025 \cdot h^3$
36.5	37	37.49	$-0.124446 + 0.081256 \cdot h - 0.001933 \cdot h^2 + 0.000034 \cdot h^3$
37.5	38	38.49	$-0.232142 + 0.103519 \cdot h - 0.003053 \cdot h^2 + 0.000055 \cdot h^3$
38.5	39	39.49	$-0.029622 + 0.074514 \cdot h - 0.001407 \cdot h^2 + 0.000026 \cdot h^3$

Za određivanje zapremine po jednosantimetarskim debljinskim stepenima, prvo treba locirati kojem stepenu pripada stablo za koje sve vrši izračunavanje, a zatim u pripadajuću regresionu jednačinu zameniti nezavisnu promenljivu iznosom visine (h) u metrima.

2.3. Trenutni broj stabala iznosi $N/ha = n \cdot \frac{1ha}{p} =$

2.4. Trenutna temeljnica sastojine iznosi $G = \sum_1^n g \cdot \frac{1ha}{p} =$

2.5. Trenutna zapremina sastojine iznosi $V = \sum_1^n v \cdot \frac{1ha}{p} =$

n	g	v	$\frac{h}{d}$	r_s	b	l	$\frac{l}{h}$	$\frac{b}{h}$	$\frac{b}{l}$	$\frac{b}{d}$	Zp	N	G	V	n	g	v	$\frac{h}{d}$	r_s	b	l	$\frac{l}{h}$	$\frac{b}{h}$	$\frac{b}{l}$	$\frac{b}{d}$	Zp	N	G	V	
1	.	0.5													45	0.03	0.31													
2	0.05	0.5													46	0.05	0.5		1.9	3.8			.			14.5	.	752	37.6	.
3	0.04	0.38		.	3.4			0.2		14.9	.	934	37.4	354.9	47	0.05	0.42	.	.	3.8	4.7	0.3	.	.		15	.	752	37.6	315.8
4	0.02	0.21													48	0.07	0.63	63	2.1	4.2	.	0.3	.	.		14.2	13.9	.	42.8	385.6
5	0.06	0.59		.	4.4			0.2		16	.	559	.	.	49	0.04	0.33	81			.	.								
6	0.08	0.86	72	2.3	.			0.2		14.2	.	512	.	.	50	/														
7	0.07	0.57	62												51	0.04	0.38													
8	0.04	0.34													52	0.03	0.24													
9	0.03	0.24													53	0.03	0.24													
10	.	.													54	0.02	0.19													
11	0.04	0.34													55	0.04	0.38													
12	0.04	0.34													56	/														
13	0.04	0.34													57	0.05	.													
14	0.06	0.59													58	.	0.68	.	2.6	.	5.9	0.3	.	.	.	.	21.2	401	.	272.7
15	0.07	0.64	64	.	4.8	5.3	0.3	0.3	.	16.2	18.1	470	32.9	300.8	59	0.05	0.5		2	4			0.2		15.5	12.6	675	33.8	.	
16	0.03	.													60	0.07	0.78	72	.	4.8	7.9	.	0.2	.	.	.	.	.	.	366.6
17	.	.	70	.	.			.		.	16.6	.	35.8	363.5	61	0.05	0.48	84	2.1	.	7.9	.	0.2	.	16.7	13.9	612	.	.	
18	0.06	0.51	70	2	.	.	.	0.2	.	.	12.6	675	40.5	344.2	62	0.04	.		1.7	3.4			0.2		15.9	9.1	934	37.4	289.5	
19	.	0.19	.			.	0.2								63	0.07	0.68	76	.	4.2	.	.	.	.	14.6	13.9	612	42.8	.	
20	0.05	0.45		1.8	3.6			0.2		14.6	10.2	.	41.7	.	64	0.03	0.21													
21	0.04	0.38													65	0.05	0.53	83			7.1	.								
22	.	0.34													66	0.07	0.79	74	2.4	4.8	8	0.4	0.2	.	15.6	.	470	32.9	.	
23	0.06	0.54		2	.			0.2		14.6	12.6	.	40.5	364.5	67	0.06	0.54	74	.	4.4	.	0.4	0.2	0.6	16.3	.	.	.	301.9	
24	0.02	0.16													68	0.05	0.52	.			6.8	0.3								
25	.	0.27													69	.	0.69	69			.	0.4								
26	0.01	0.09													70	0.04	0.35	.			.	.								
27	0.03	0.27													71	0.03	.	88			5	0.3								
28	.	.	.	.	5.2			0.2		.	.	.	36.1	364.9	72	0.05	0.41	78	2	4	5.6	0.3	.	.	16.5	12.6	.	33.8	276.8	
29	0.04	0.34													73	/														
30	0.11	1.18	65												74	0.05	0.39	75			5.9	.								
31	0.05	.	87			6.9	0.3								75	0.06	0.52	63												
32	0.05	0.47	.			7	0.3								76	0.1	1.1	.												
33	0.07	.	.			6.2	0.3								77	0.06	0.54													
34	0.01	0.08	143			.	.								78	/														
35	0.04	0.34													79	0.05	0.5													
36	.	0.42													80	0.02	0.19													
37	0.06	0.59													81	0.08	.	71	3	6			0.3		18.9	28.3	300	.	252	
38	/														82	0.05	0.42													
39	0.03	0.21	84			.	.								83	0.04	0.38													
40	0.06	0.54		2.3	4.6			0.2		.	16.6	.	30.7	276.5	84	0.04	0.38													
41	0.05	0.45		1.8	.			0.2		.	10.2	833	41.7	.	85	0.07	0.6	65	2.3	4.6			.		.	.	512	35.8	.	
42	0.05	0.5		2.3	.			0.2		.	16.6	.	.	256	86	0.03	0.27	94			5.6	0.3								
43	0.06	0.52	.	2.5	5			.		.	19.6	434	26	225.7	87	0.04	0.38		1.9	.			.		16.4	11.3	752	.	285.8	
44	0.05	0.45		.	.			0.2		16.9	13.9	612	.	275.4																